

# Using Frontera for the Direct Numerical Simulation of Hypersonic Flows

Daniel J. Bodony, Bryson Sullivan, and Fabian Dettenrieder  
Aerospace Engineering

January 28, 2021



Dr. Sarah Popkin  
FA9550-18-1-0035



# A Definition of Hypersonics



X-51 Waverider (Mach 5)



HTV-2 (Mach 20+)

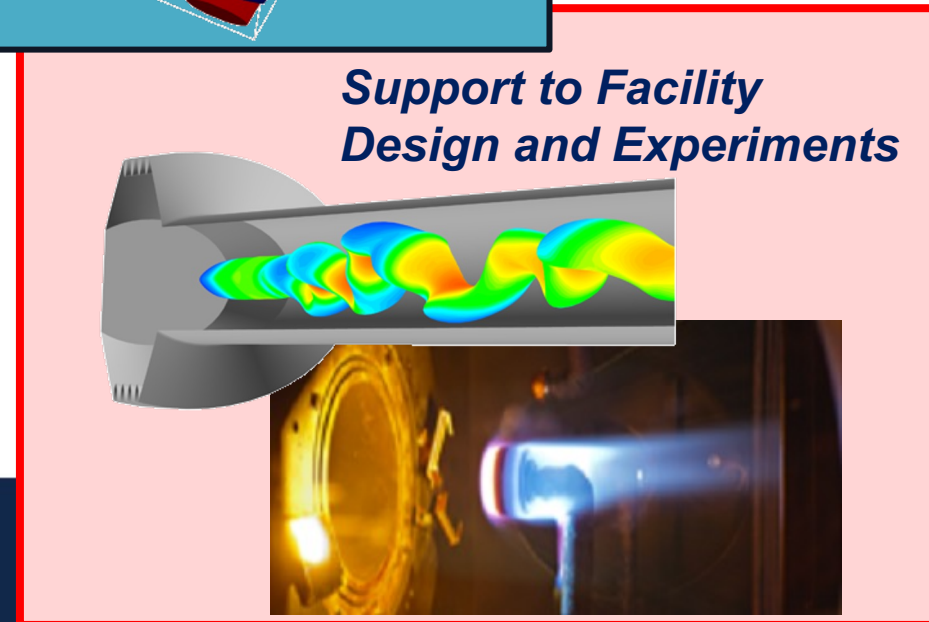
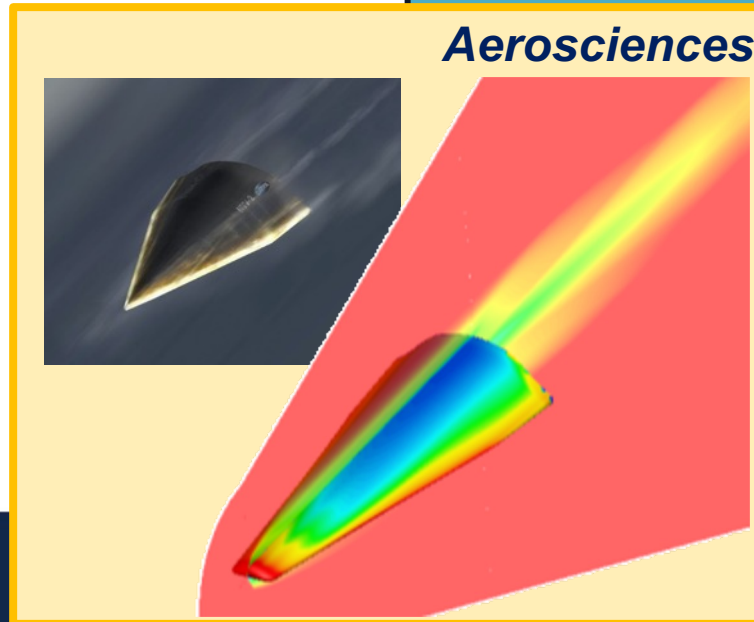
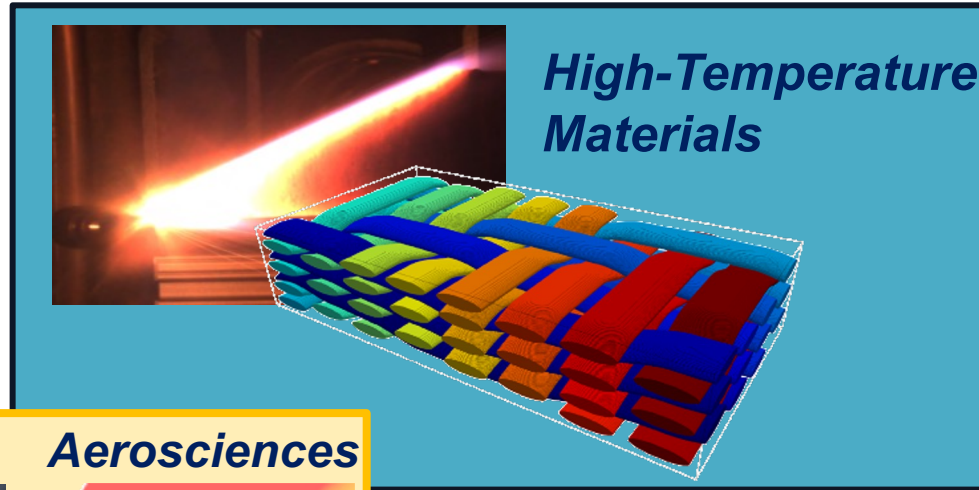


Stardust (Mach 43)



Mach #:  $M = \frac{\text{velocity}}{\text{speed of sound}}$

# Modeling Challenges



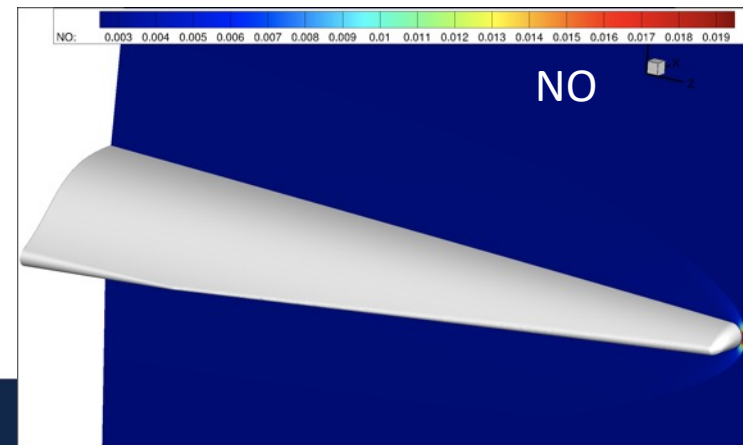
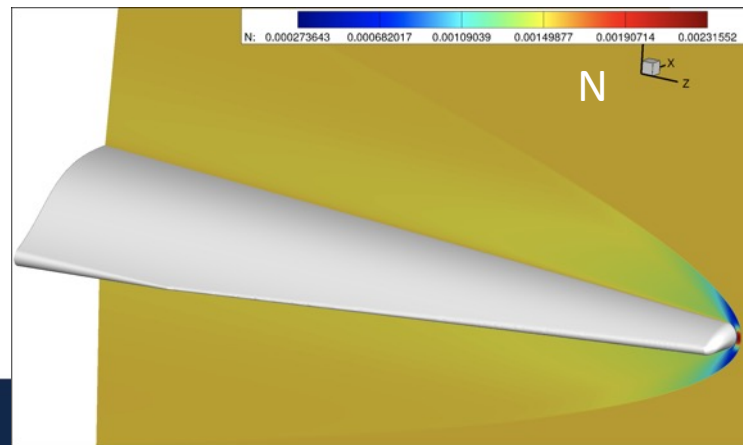
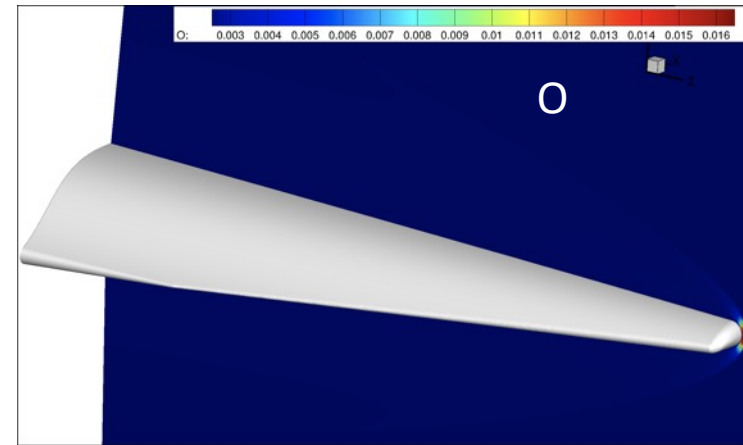
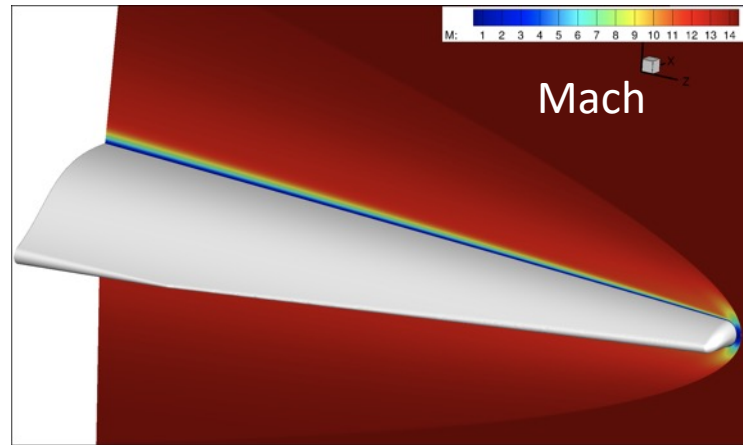
# Hypersonics: An HPC Grand Challenge

- Multiscale in space:  $10^{-9}$  to  $10^1$  m
- Multiscale in time:  $10^{-10}$  to  $10^2$  s
- Domain-specific codes (MD, DSMC, FEM, CFD, rad, E&M)
- Different codes map differently onto heterogeneous hardware
- Inter-code orchestration
- UQ & MDO need multiple realizations
- (Didn't even discuss I/O...)



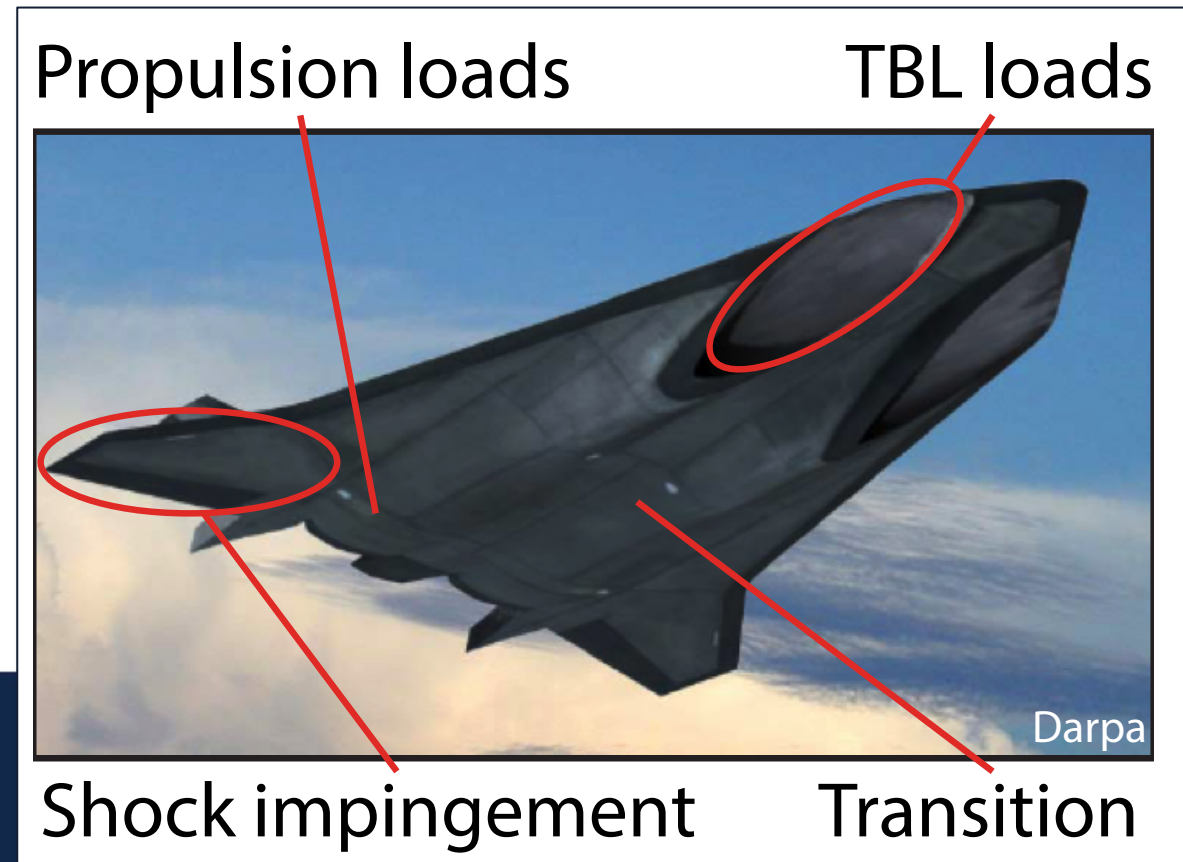
# Example Mach 15 Flow Field

5-species air, 100 kft, 800 Frontera nodes



# Aerosciences: Key Understanding Gap

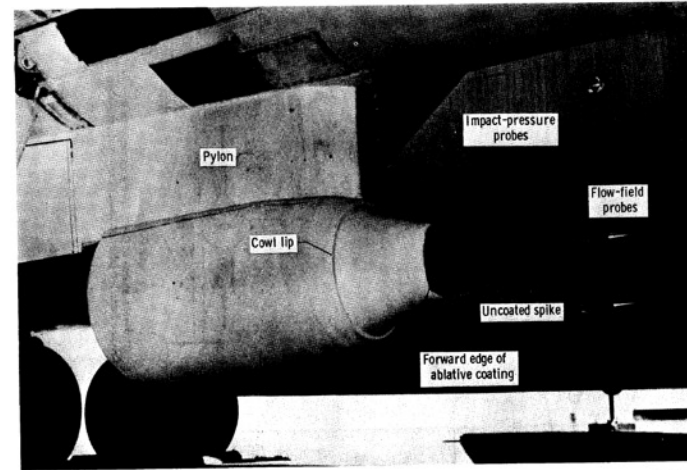
- Extracted from Boeing and Lockheed pre-PDR designs of Mach 5-7 reusable vehicle (AFRL-RB-WP-TR-2010-3068, -3069, and summarized by Eason et al., AIAA Paper 2013-1747).
- “Can only approximate the acoustic environment ...”
- “Identification of critical thermal, mechanical, and acoustic loads ...”
- “Predicting aero-elastic characteristics of thin metallic structure at high T ...”



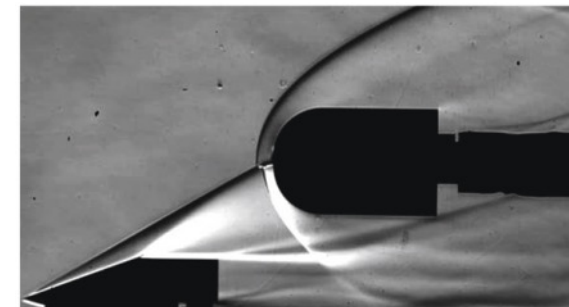
# Case Study 1



X-15-2 carrying pylon-mounted dummy scramjet  
Credit: USAF



Unanticipated shock-shock interaction caused loss of “engine”, severe damage to pylon (Watts, 1968)



Edney Type IV shock-shock interaction leads to localized intense impinging jet (Chettles et al., 2005)

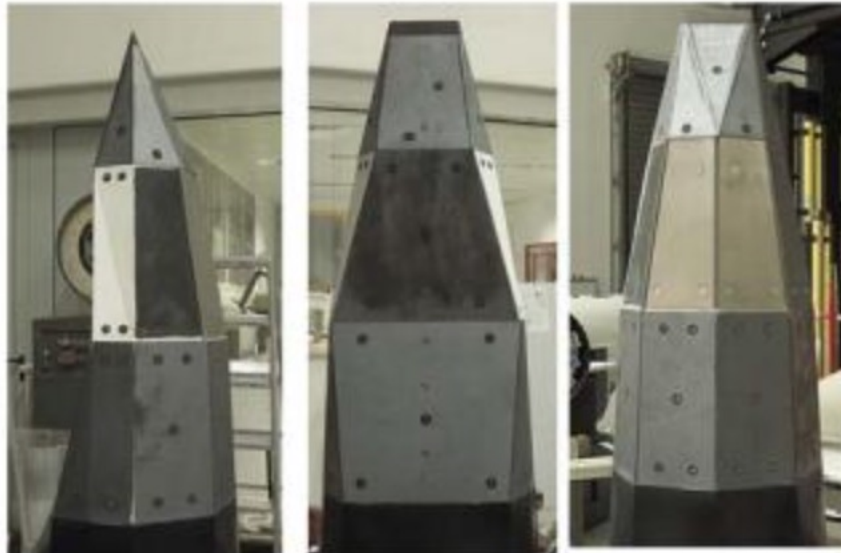


# Case Study 2

- SHEFEX-I (Sharp Edge Flight Experiment) by DLR in 2005
- Purpose: test flat-sided design and TPS concepts for re-entry vehicles



Launch from Andoya, Norway



Vehicle nose carried primary experiment of flat paneled hypersonic structure



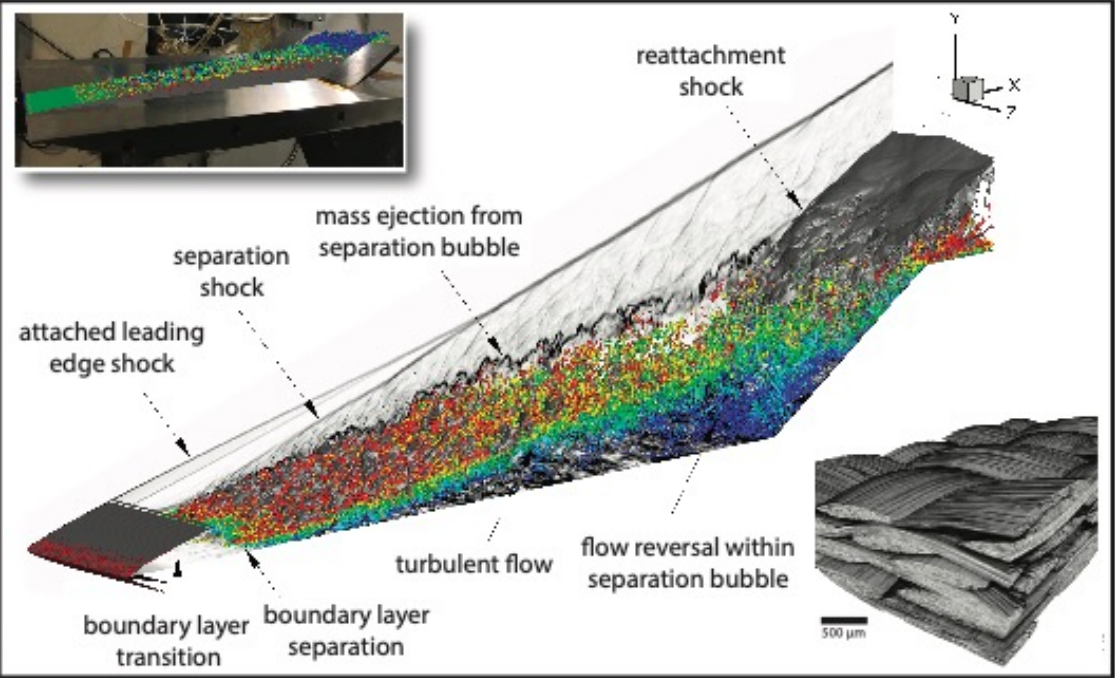
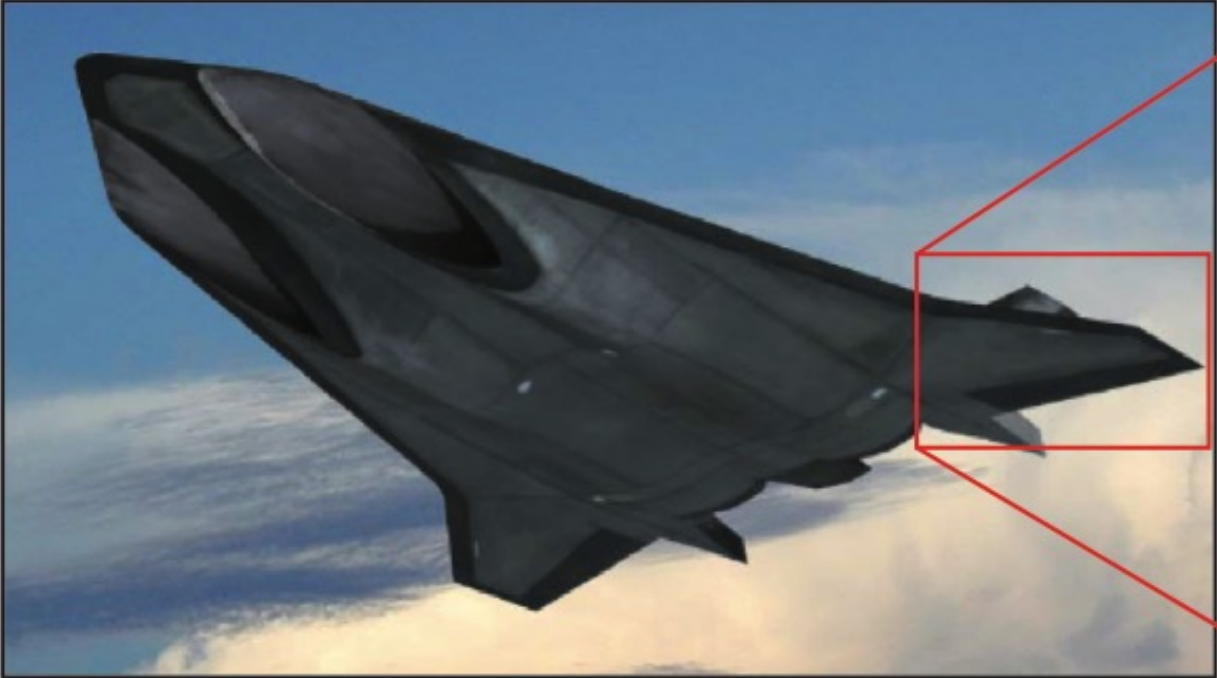
Rear section of SHEFEX-I during decent. Circles indicate control surface LE deformation due to FTSI.



# Frontera: Study FSI of a 35 deg ramp

TBL Loads

Propulsion Loads



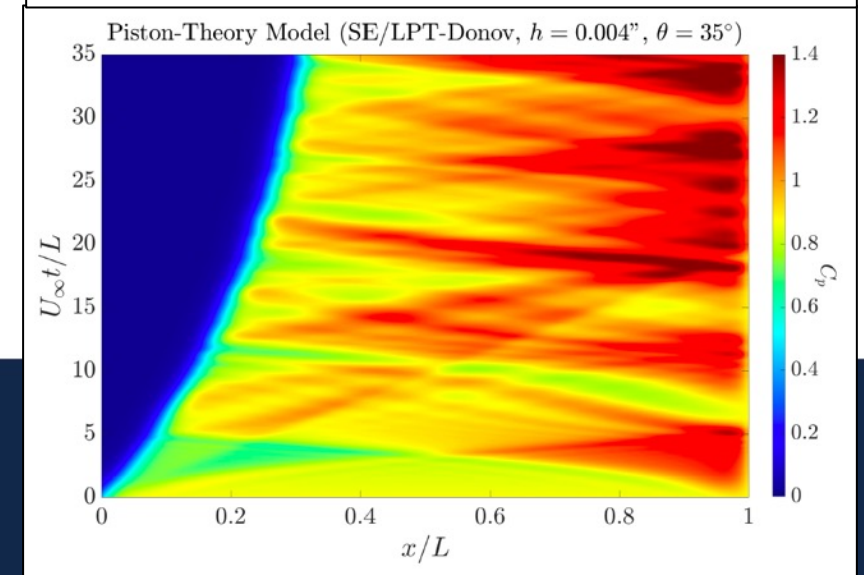
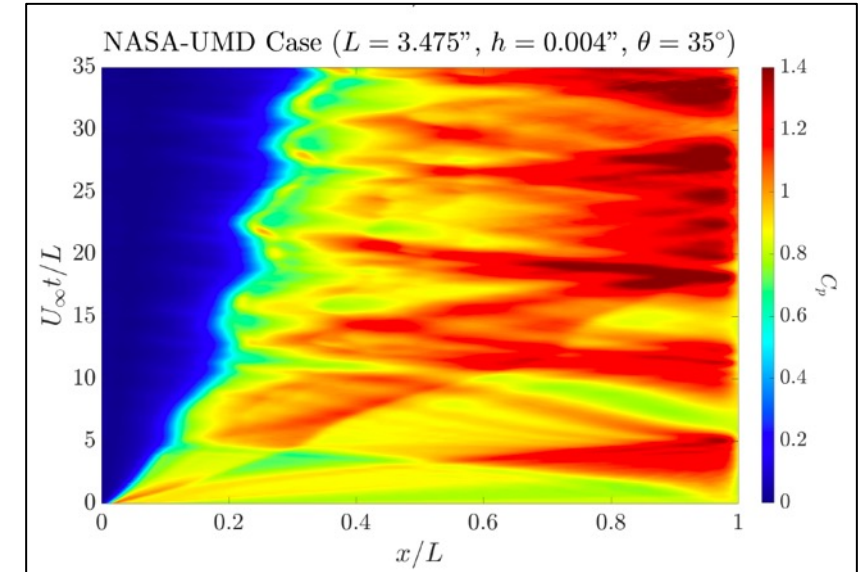
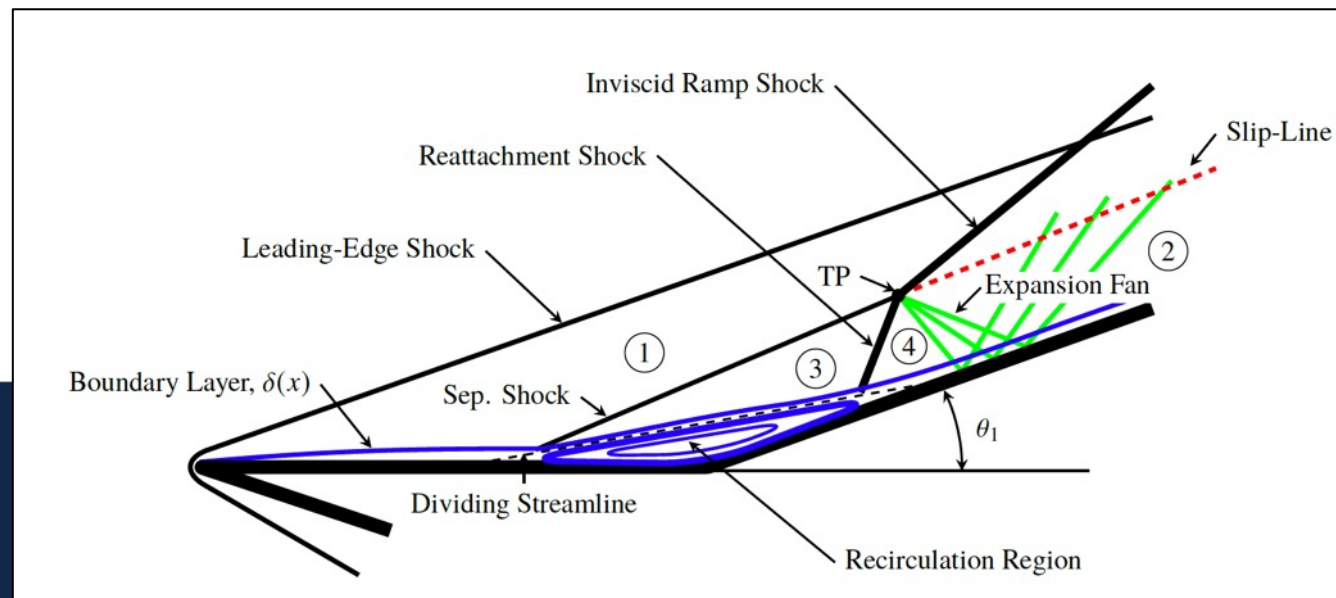
Transition

Shock Impingement



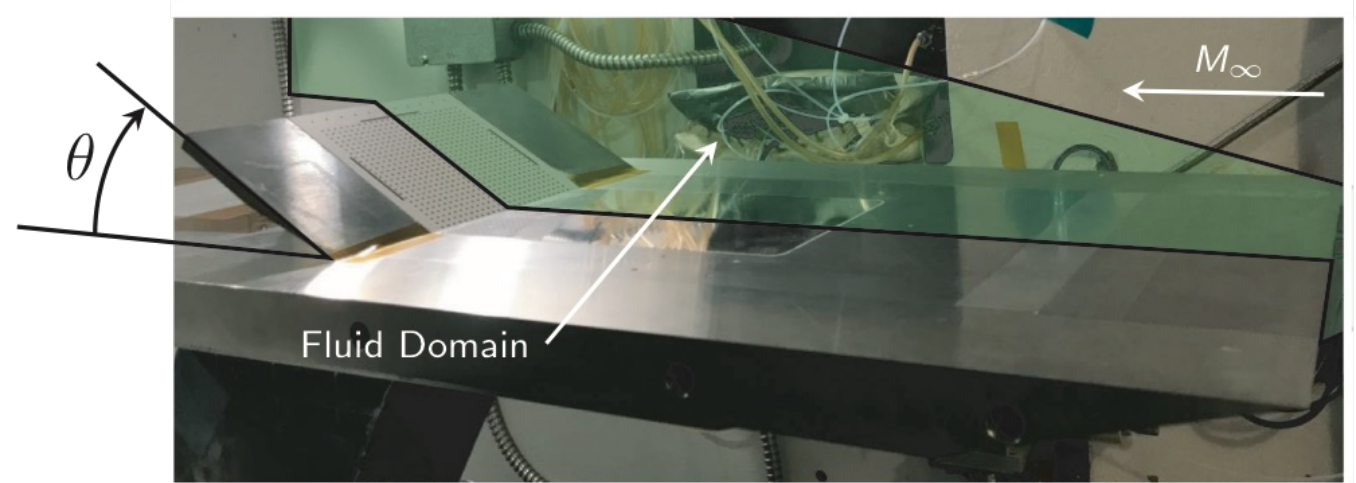
# Goal: Useful Reduced-Order Model

- Fluid prediction dominates cost of FTSI DNS
- Also represents the biggest unknown in OEM design and analysis
- Developed a multiple-shock version of local Piston theory (Sullivan et al., AIAAJ, 2020)



# High-Speed FTSI: Shock on Control Surface

- Flow conditions:
  - Mach 6
  - $T_0 = 522$  K
  - $P_0 = 3.2$  MPa
  - unit  $Re = 23.6 \times 10^6 / m$
- Model conditions
  - 4140 stainless steel plate
  - milled compliant section
  - 0.032" tested



Credit: Tom Whalen and Stuart Laurence (UMD)

- Test time  $\sim 5$  sec
  - Tunnel started with model retracted
  - Model raised in  $\sim 3$  sec
  - Data collected for  $\sim 5$  sec



# Computational Approach

Coupling:

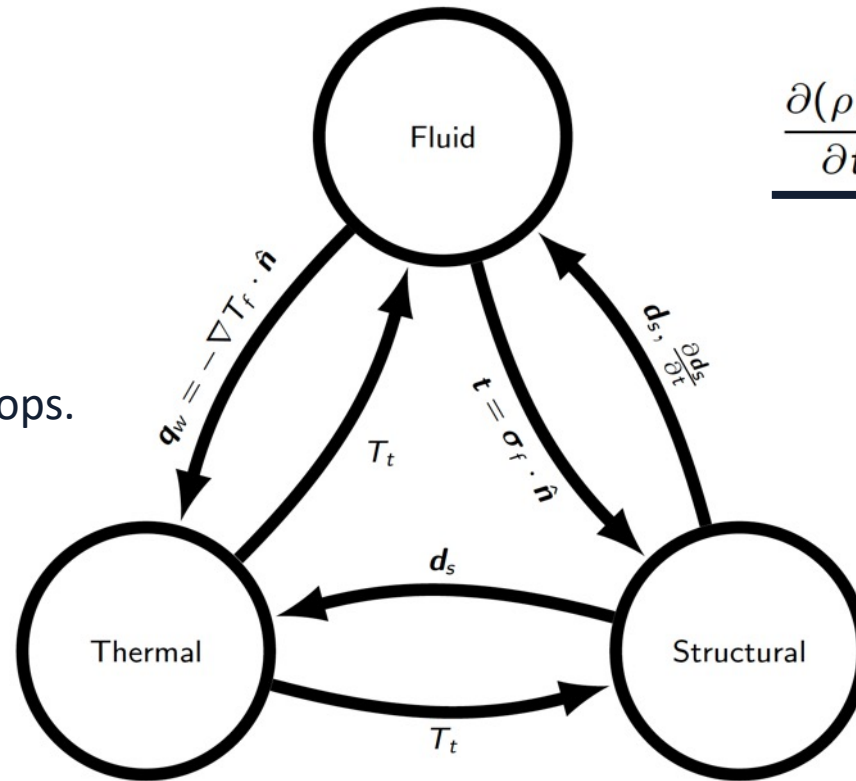
- C++ MPI layer
- Multirate time advancement

Material model:

- Isotropic
- Compressible Neo-Hookean
- Temp. dependent material props.

$$\rho C \dot{\Theta} + \nabla \cdot \mathbf{q} = 0$$

Quadratic FE  
Crank-Nicolson



$$\frac{\partial \rho}{\partial t} + \frac{\partial(\rho u_j)}{\partial x_j} = 0$$

$$\frac{\partial(\rho u_i)}{\partial t} + \frac{\partial}{\partial x_j}(\rho u_i u_j + p \delta_{ij} - \tau_{ij}) = 0$$

$$\frac{\partial(\rho E)}{\partial t} + \frac{\partial}{\partial x_j}[u_j(\rho E + p) + q_j - u_i \tau_{ij}] = 0$$

Finite difference SBP-SAT + WENO  
Generalized, deformable coords.

$$\nabla \cdot \boldsymbol{\sigma} + \rho_s \mathbf{b} = \rho_s \ddot{\mathbf{d}}$$

Quadratic FE  
Multiplicative Split  
Newmark-Beta

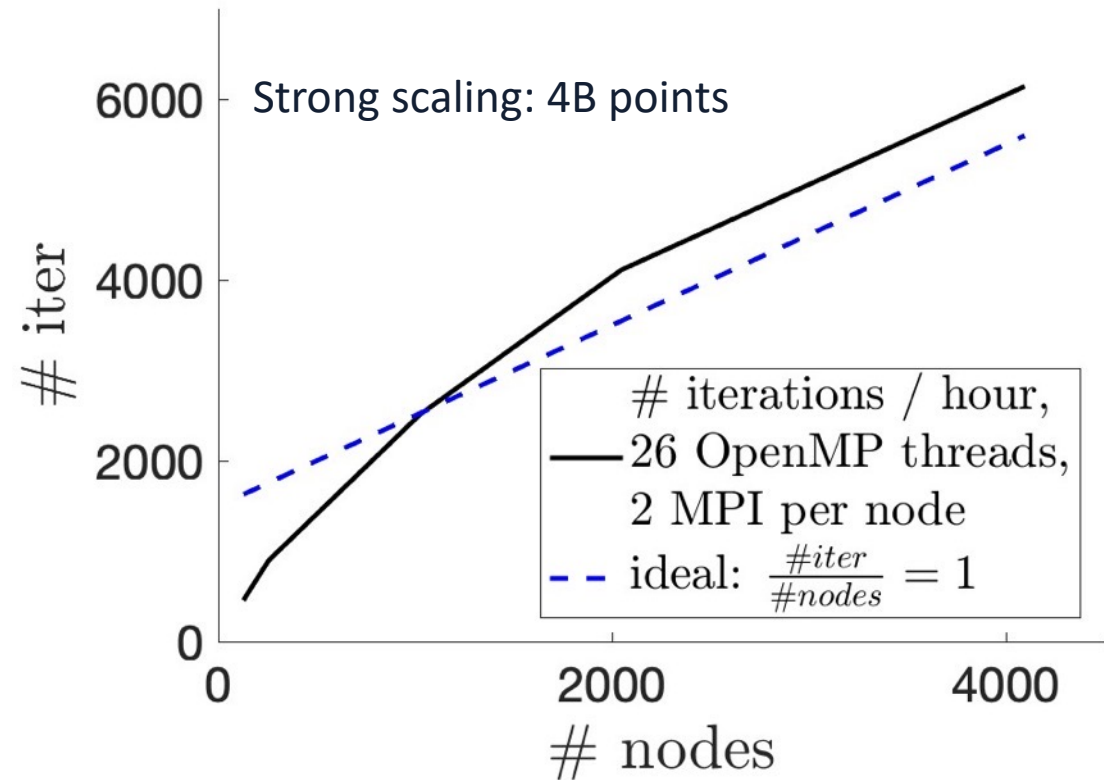
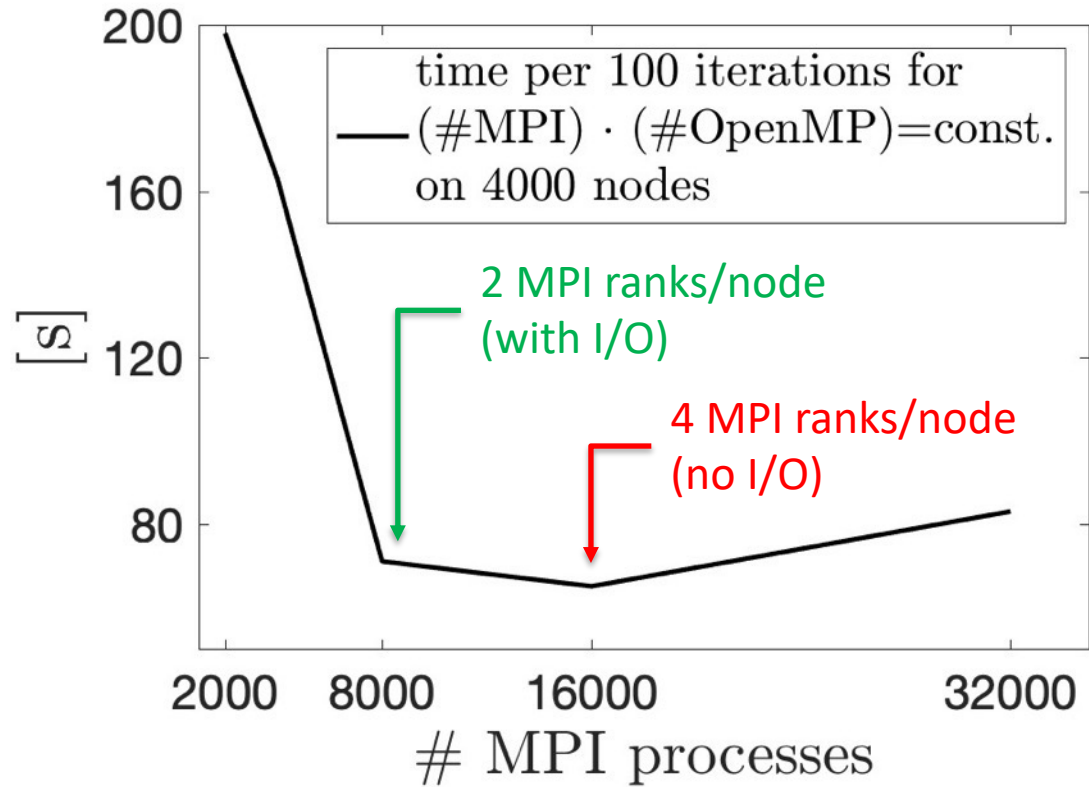


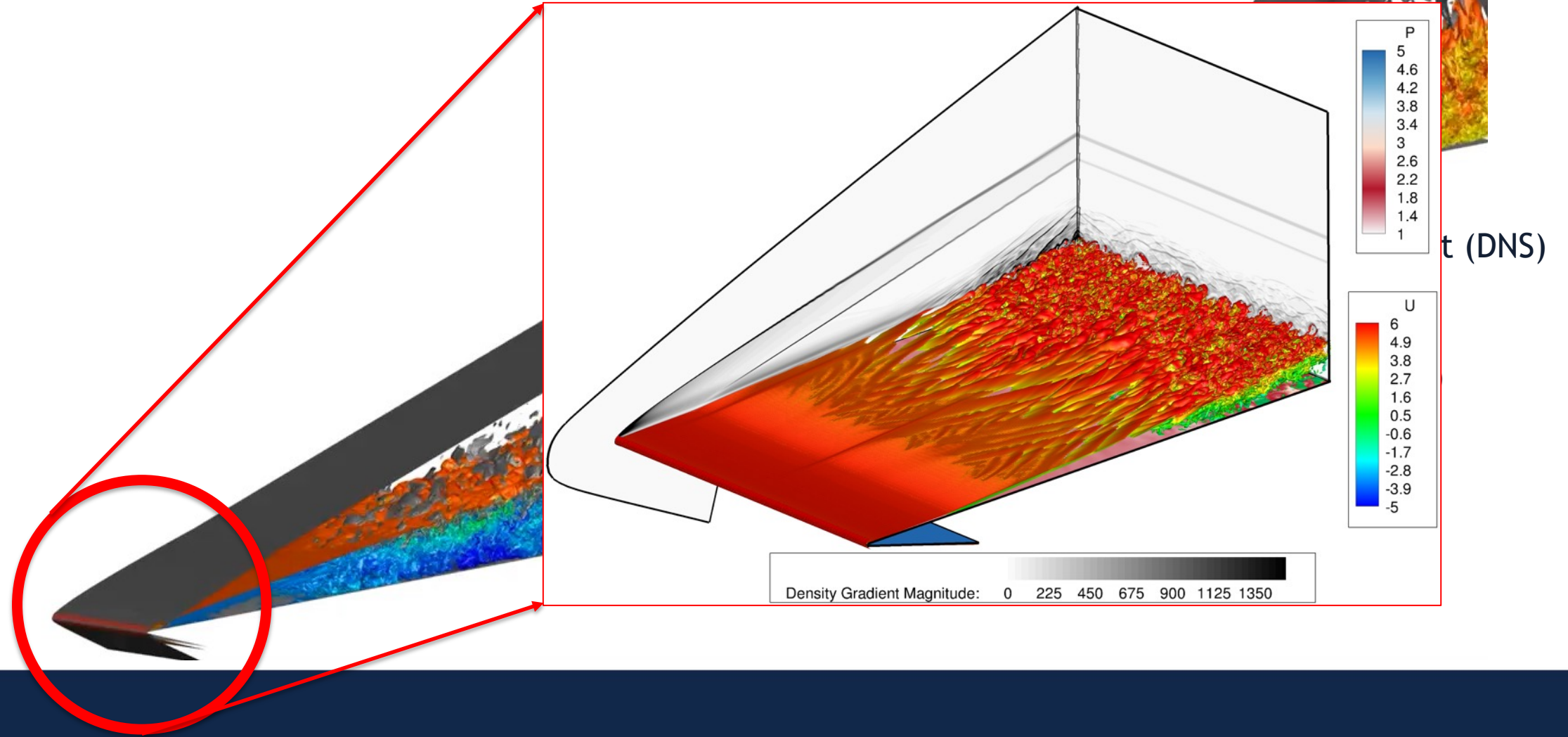
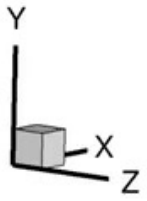
# Computational Infrastructure

- Additional Capabilities
  - Multi-rate time integration
  - Structured overset
    - Geometric flexibility
    - Deformable / moving
  - Different grids = different physics models
  - Cantera-informed chemistry (Prometheus)
  - Multiphysics linear operator (global modes, input/output, resolvent analysis)
- Code details
  - C++ infrastructure
  - Physics kernels – extensible
  - MPI + OpenMP ( $\geq 4.5$ )
  - GPU offloading via OpenMP
- Thermo-mechanical
  - Built on MFEM
  - Includes TPS models, radiation, ...



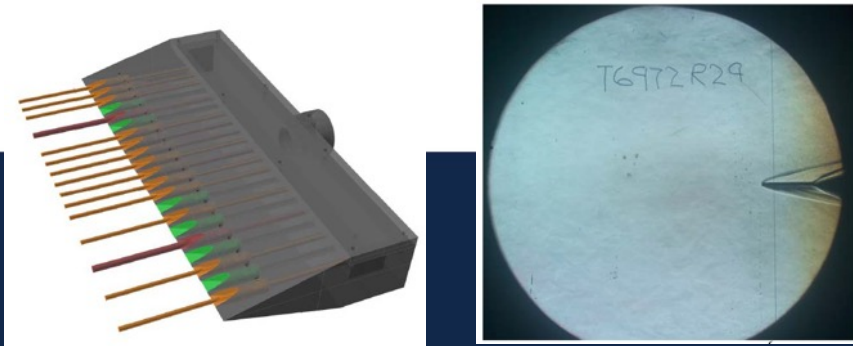
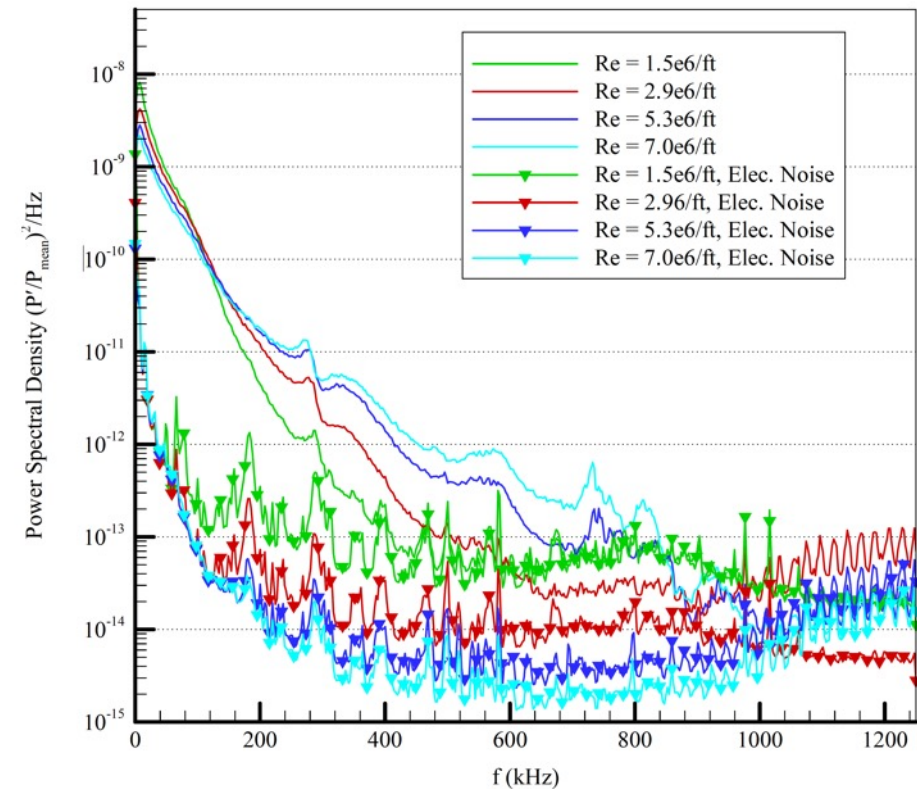
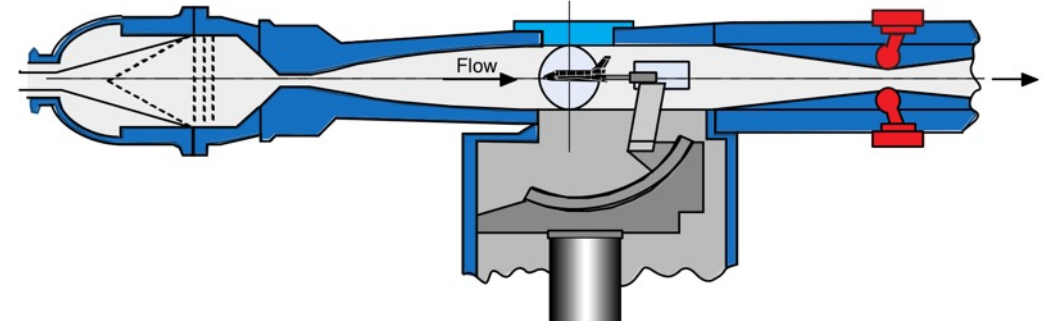
# Performance on Frontera





# Return to NASA LaRC M6 Tunnel Details

- Tunnel walls are flat and radiate sound
- Sound impacts model:
  - Modifies flat plate boundary layer transition
  - Changes FTSL
  - No diagnostics to suggest where BL transitions
- Resort to including acoustic field in the 3D calculations
- Rufer & Berridge (AIAA 2012-3262)





# Model NASA LaRC M6 Tunnel Noise

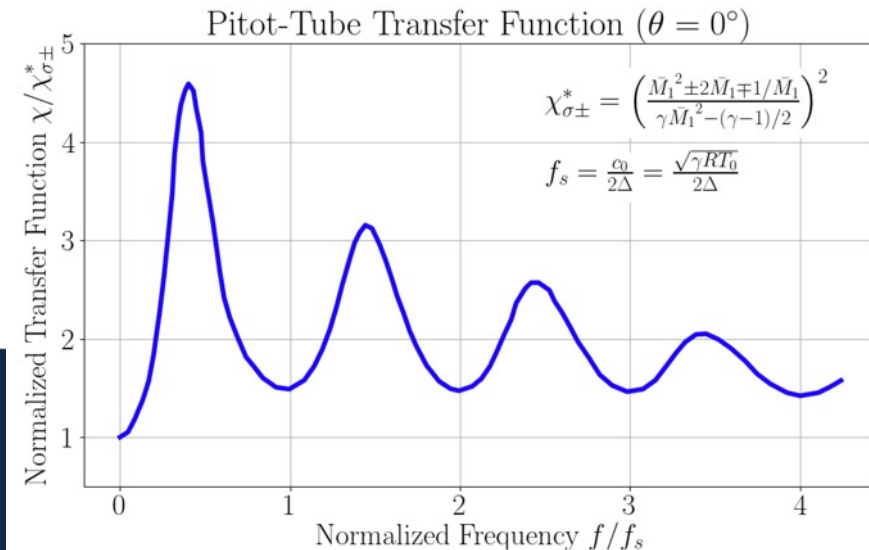
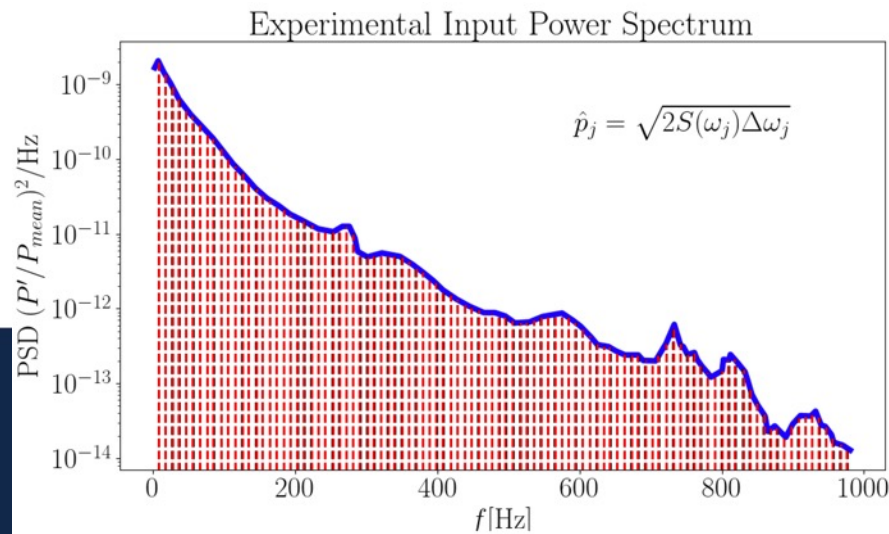
- Take measured PSD from Kulite / PCB rake
- Apply Tam *et al.* PSD discretization
- Apply inverse pitot-tube transfer function (Chaudhry & Candler)
- Assume plane wave field:

$$p'(\mathbf{x}, t) = p_\infty \sum_{j=1}^{N_w} \hat{p}_j e^{i(\mathbf{k}_j \cdot \mathbf{x} - \omega_j t + \tilde{\phi}_j)}$$

$$= p_\infty \sum_{j=1}^{N_w} \left( \sqrt{2\hat{S}(\omega_j) \Delta\omega_j} \right) e^{i(\mathbf{k}_j \cdot \mathbf{x} - \omega_j t + \tilde{\phi}_j)}$$

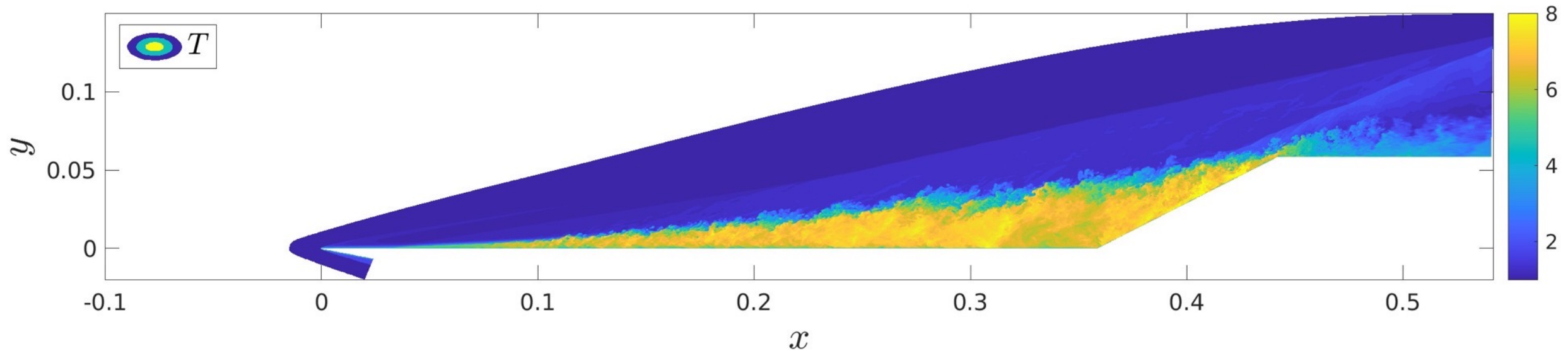
$$p'(\mathbf{x}, t) = \frac{1}{c_\infty^2} p'(\mathbf{x}, t) = \frac{1}{\gamma} \sum_{j=1}^{N_w} \hat{p}_j e^{i(\mathbf{k}_j \cdot \mathbf{x} - \omega_j t + \tilde{\phi}_j)}$$

$$\mathbf{u}'(\mathbf{x}, t) = \frac{c_\infty}{\gamma} \sum_{j=1}^{N_w} \hat{p}_j \frac{\mathbf{k}_j}{\|\mathbf{k}_j\|} e^{i(\mathbf{k}_j \cdot \mathbf{x} - \omega_j t + \tilde{\phi}_j)}$$



# 3D DNS with NASA LaRC M6 Tunnel Noise

- 6 Billion grid points
- Running on NSF Frontera with 1024 nodes (57K cores)



# Summary

- There are many FTSI scenarios that are critical for hypersonic flight
- Historical use of noisy ground tunnels may impact our FTSI models at flight conditions
- Fundamental investigations coupled with good modeling (cf. McNamara) and recent experiments (cf. AEDC) are going to impact our understanding of FTSI at high Mach numbers
- Much work is needed on “basic” flows



# Contact Information

Daniel J. Bodony

Blue Waters Professor

Department of Aerospace Engineering

Department of Mechanical Science and Engineering (by courtesy)

306C Talbot Labs

104 S. Wright St.

Urbana, IL 61801

T: (217) 244-3844

[bodony@illinois.edu](mailto:bodony@illinois.edu)

<http://acoustics.ae.illinois.edu>